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EXPERIENCES WITH ICE IN STANDPIPES¹

By Leonard Metcalf²

Some time ago the author was confronted with the question as to whether it was necessary or not to house standpipes in northern New York, under certain conditions of exposure and circulation, in order to maintain satisfactory service without dangerous risk from the effect of the formation of ice in them. The housing of the standpipe bade fair to nearly double its cost, and the tremendous increase in the cost of water works construction of all kinds, particularly of steel structures, made it necessary to save expense in every desirable way.

It was thought that past experience with such structures in the northern United States and in southern Canada might furnish an answer to some of the important practical questions involved, and aid in reaching a sound conclusion. Therefore a questionnaire was sent out (February 18, 1920) to about 300 northern water works having standpipes, relative to their past experiences in operating them during the cold winter months. The response of the superintendents to this questionnaire has been so prompt and courteous, and the experience outlined is so suggestive, that the author has thought it desirable to bring the assembled information before the water works fraternity, for the convenience of these men, and other superintendents and engineers who may be interested in the subject, in the form of a permanent record available to all.

The replies received have been classified in the accompanying tables in three groups under two main classes as follows:

Group Ia. Ground water supplies with encased standpipes
Group Ib. Ground water supplies with roofed standpipes
Group Ic. Ground water supplies with uncovered standpipes
Group IIa. Surface water supplies with encased standpipes

Group IIb. Surface water supplies with roofed standpipes Group IIc. Surface water supplies with uncovered standpipes

Discussions of this paper are desired and should be sent to the Editor.

² Of Metcalf & Eddy, Consulting Engineers, 14 Beacon Street, Boston, Mass.

It is to be noted unfortunately that the question as to whether the supplies were drawn from the ground or from the surface, was inadvertently omitted from the questionnaire, and that lacking time to recanvass the situation, this information was drawn from the "McGraw Water Works Directory" (1915).

The reasons for the grouping adopted are obvious. Ground water is generally more equable in temperature, colder in summer and warmer in winter, than is water obtained from surface sources. The three groups, "encased," "roofed" and "uncovered," were thought likely to differentiate the effect of covering the standpipe.

One hundred and twenty-seven replies were received, falling within the following groups:³

Group Ib.	Ground water with encased standpipes	39	
Group IIa. Group IIb.	ound water supplies Surface water with encased standpipes Surface water with roofed standpipes Surface water with uncovered standpipes	11	67
Total sur	face water supplies		60
Grand tot	al replies received		127

Supplementary Information Submitted with Replies to the Questionnaires

Long Beach Water, Company, New York; L. W. F. Carstein, Manager. In general our experience leads us to infer that heavy ice formations will occur within the standpipe. The tumbling of ice is frequently heard. It would seem that with the constant lowering and raising of the water level, together with occasional thaws, the ice formation cracks and breaks up and tumbles to a lowered water level. No damage or annoyance, however, has been experienced therefrom. The writer would expect to find by actual observation, that a heavier ice formation would be found on the north and westerly exposure than on the southern exposure, owing to the prevailing northwesterly winds, and again to the moderating action of the sun's rays during the total period of sunlight.

Winchester Water Commission, Massachusetts; William T. Dotten, Superintendent. We have two (standpipes). One concrete, built about 8 or 10 years... Ice forms on the walls or sides from 12 to 15 inches. In cold winter five or six years ago we opened in May the manhole at the bottom and removed (estimated) 60 tons of ice. It was a foot thick on the north walls

³ Later information indicates that certain of the supplies in groups 1A, 1B and 1C should be classified rather as surface waters.

METCALF & EDDY consulting Engineers BOSTON-MASS. WITH ICE EXPERIENCES IN DATA OBTAINED BY METCALF & EDDY, FEB. MAR. 1920 FROM AND BY THE Date of constructio je je Material of On grou Kind of Encasing Encased for Architectural Pagt. Height of or hill Authority Construction or on Location roof tower Place tower. Height GROUP IA. GROUND WATER SUPPLIES WITH Concr. fdn. 1910 Steel 80 Exposed Wooa No Jas. Scholes, Supi 20 WEYBURN, SASK. Ossining . N.Y. Jas Bedell, Supt. 1889 Wrought Iron Reinf. Concrete 30 Ground Exposed iron (1) No OSSINING . N.Y ROUND LAKE, N.Y. Ground Stone Wall Exposea In Trees No No Jas. Bedeil, Supt. 1909 26. 55 Concrete (2) (3) J.T. Wilmot 1890 Wooden 25 15 8ft. Wood & Tin (Conical Wood Metal clad NORTH BATTLEFORD, SASK M.D.Cadwell.Supt Steel 20 80 Ground Exposed No (4) WATER SUPPLIES WIT GROUP IB. GROUND 1. NEWAGO, MICH.
2. BELDING, MICH.
3. DUXBURY, MASS.
4. FERGUS, ONT.
5. CHERRY VALLEY-ROCHDALE 1913 Wooden 20 18 Tower 85 ft. 80 ft. In Open G.M.Burner, Supt Metal Concr.Dome None P.A. Frederick Supl Steel 20 1905 L.M. Peterson, Sup 1914 Concrete 40 Ground 30 ft No Water Dept. Water Dist. Water Dept. 90 ft. Exposed None Tower Iron 1912 Steel 21 Ground Brick bas 1910 1900 Concrete Steel 40 21 Exposed Exposed Concrete No 59 ft. Water Dept.
H.G. Cokes
D. V. Wardrer Nag.
Wat Light - Pow Co.
Water Dept. ANSING, MICH. IRR5 Steel IR 152 Ground Exposed In Open Wooden Stee! Sheet Metal 1908 16 /25 Ground MUSKEGON HEIGHTS. MIC 100 ft. 9. CASS LAKE, MICH.
10. WRENTHAM, MASS. Steel 20 30 Tower Exposed Exposed Metal Riser Encasea No 1910 Ground 1907 Steel Steel II. MILFORD, MASS.
12. WINCHESTER . MASS. J. Wm. Kay. Supt. W.T. Doten, Supt. 1912 Steel 24 30 Ground Exposed Stee! 40 67 None 27 25 1910 Concrete 13. PLAINVILLE, MASS.
14. UBLY, MICH.
15. BROOKLINE, MASS. In Trees Water Dept. Water Dept. 1908 1913 Steel Steel Cement fål Steel N'one No 20 Tower 75 ft. Sheet Iron Waqqicayerea Riser Encased Water Dept 1889 Wrought Iron Wrought Iron 50 30 Ground Ground Exposed No L.M.Bancroft, Supt. 16. READING , MASS. 17. AMENIA , N.Y. 18. BEDFORD , MASS. 30 100 Exposed In Trees 1890 Water Dept. 1891 Wooden 24 24 Ground (Stone and Concr. fain. Ground Shinale 100 100 Wooden Wood and Proofing Page Netal Cone 20 7*ft*. Exposea In Open G.M.Dimond, Supt. 1908 Steel No 19. MARSHALL, MASS. 20. FRAMINGHAM, MASS. P.S. Joy, Supt. Water Dept. 1890 Steel 20 40 Steel 81 Ground Exposea Exposed Knor Roof Ground 21. BALDWINSVILLE, N.Y Ezra Cole, Supt. 1889 Wrought Iron 20 50 None NO Wooden Wrought Iron Steel No Na No Na OUT 20 Conical Wood (Flat 2 plank (stringers in al Metal Brick Towe Terrace In Open In Open 22. ORILLIA, ONT. Warter Dept. 18 20 75 204 None 23. BATTLE CREEK, MICH. 7. 24. RIVERHEAD, N.Y. 25. ASHLAND, MASS. Water Dept. Water Dept. Water Dept. Water Dept. 1887 18 6 ft 180 ft Lincl ta In Open
Exposed
In Open
In Open
In Open
In Open
In Trees
In Open Tower 1915 40 3/ Cement 1911 Concrete Ground 26. NORTH ATTLEBORO, MAS 27. MATTAPOISETT, MASS. 28. SAUGATUCK, MICH. 40 28 60 ft. 1884 Wrought Iron Steel 60 90 Ground Steel None Conical Stee. None Water Dept. 1913 Ground Water Dept. Concrete None Ground Shingical No No 1900 H.H.Pieroe, Supt. L.W.F.Carstein, Mgi 29. BARNESVILLE, MINN. 30. LONG BEACH, N.Y. 1908 Steel 25 105 Tower Stee None Exposed In Open In Trees 34 50 Steel 150 Concrete filin 3ft Cone shap Proba 30. LONG BEACH, N.T.
31. MANCHESTER-BY-THE-SEA,
32. LITTLETON, MASS. (MASS.
33. CLOQUET, MINN. Gustavino 1909 Concrete None G.F.Evans . Supi 72 Ground Steel Steel Ground Tower Water Dept 1911 1908 35 40 28 Steel Pitch Exposea 137 ft. Wood Riser Enc**ase**a Water Dept. W.O.Neil. Supt. 24 33 CLOQUET, MINN.
34 LAKE GENEVA, MICH.
35 WATERTOWN, WIS.
36 MONUMENT BEACH, MASS
31 ELMIRA, ONT.
30 BANGOR, MICH. (W. O'Neil. Suot. Water 6-Lt. Comm. Water Dept. Wooden 20 18 38 80 Brick fain Shing'e Steel None 1890 None 30 ft 190 ft linc tan 90 ft Exposea 1895 Stee! Ground T.Chaffin,Supt Water Dept Water Dept Steel Chicago Nettle shi Steel al.cap) Tower Riser Enca (Supply Pipe (Encased None 1916 1908 n na Exposed Wrought Iron Nα Exposea In Open m 16 18 Tower Meta No Tower Tower 100 :: 1893 Steel 39. SPENCERPORT, N.Y. Water Dept. Steel Exposea Riser Encasea GROUP IC GROUND WATER SUPPLIES N 1. BOYNE CITY, MICH. I. 2. BOYNE CITY, MICH. 2. 3. BOYNE CITY, MICH. 3. 4. NEW ROCHELLE, N.Y. H.H.Tinker, Supt. H.H.Tinker, Supt. 86 50 Two open One Nood 150 Concrete Ground 215ft.hill Exposed 190G-10 None H.H.Tinker, Supt. F.T.Kemble, Supt. 30 60 60 60 Ground 30ft.his Exposed 1895 Steel Wrought Irun Steel Exposed Exposed 5 SHARON, MASS E.E.Farmham,Supt. 80 126 Ground None None 1085 LOCKPORT. N.Y. AMITYVILLE, N.Y. SPENCER, MASS. BRAINTREE, MASS. Ground Ground Water Dept. 1909 25 None Exposed Exposed Exposed In Trees Water Dept. Water Dept. 1893 1899 Wrought Iron Steel 20 40 125 None None Ground (Brick and Cement tain. Concrete faln. W.L.Gage. Water Dept. 1887 Wrought Iron 40 100 6ft None 10. CORTLAND . N.Y.
11. TISBURY , MASS
12. WOLCOTT , N.Y.
13. ANN ARBOR . MICH Ingot Iron Exposed None 60 1911 Wrought Iron Steel J.E.Howland, Supt. B.J.Christian, Supt. 1885 1912 20 15 50 85 Ground Ground Exposed Exposed None None None R. Spokes, Supt. Water Dept. Water Dept. 1916 1890 Steel Steel 30 18 60 Tower In Open None 13. ANN ARBUN, MICH

4. MOHAWK, N.Y.

15. MANISTEE, MICH.

16. BROOKLYN, N.Y. FLATBUSH W.W.Q.

17. NANTUCKET, MASS.

18. KALISPELL, MONT. Graund Exposed None 50 55 Ground Ground None 1912 Steel 45 80ft.hill Exposed 20 EH.Lott, Supr 1881 Exposea None Steel Ground Concrete fa Exposea Shelterea None Nane Wannammet W Co iana Steel 30 80 Vane 1892 Steel 19. RIPON, WIS. Cent WistHilities Co. Wrought Steel 1895 15 100 Ground In Open Nane None 40 76 55 20. WAUKESHA, WIS. B.B.Haifford, Supt 1887 35 Ground 128 ft. In Open In Trees None None 21. WINCHESTER, MASS 22. BARABOA, WIS. WT Doten, Supi 40 30 /AGA Steel Ledge Ift. None None None Water Dept Ground Exposed 23 FRANKLIN MASS F.A.Darling, Supt. IÀA 4 lmn 80 Ground Exposea Nane None (1) 12° Brick tower 2.5t. between wall and tank. (2) Rubble wall 2'.9° thic (5) Nood stove, with fire morning and evening when temperature is below zero. (9) Lumber with 2ft. air space. (0) Cost of casing about 30 % of whole.

(2) Rubble wall 2'9" thick at base; 15" to 20" at top; 12" air space

(6) Small radiator in bottom of standpipe all winter.

^{*} Later information indicates that certain of the supplies in Groups 1A, 1B and 1C shou

of.	Encasing tower	d for ctural only?	oipeaut in winter ?	Thicknes in ordinar			s of ice in nany weath.	project	ificial applied?	Has pipe suffered injury from ice ?	attional 50 % to protection de
		Encased for Architectural effect only ?	Is standpi of service i	On top of water	On inside of shell	On top of water	On inside of shell	Does ice, above, pi,	is artificia heat applie		Is addition to so to so to so to so to so so for properties of the solution of
2 ج	SUPPLIES 1	WITH .	Ενα	ASED	STANI	PIPES	*				
	(9) (1) (2)	No No No	No No No	Very little None More ice th	None None an in Wroug 6"	3 or less 2 ° ht iron Sta	None	No Never	No No	No. Water level kept fluctuating.	(10) Yes no matter what the cost
9	(3) (4)	No No	No No	1/2"	6" None	12"-18"	None	No	No 153 30 40 days	(No. Pipe freezes so cannot use it: Used only for fire. No. Water heated to 60-70 degrees.	Yes, "absolutes
EB.	SUPPLIES	WITH	Ro	OFED	STAND	PIPES	. *				
	None	146	No No					No	No	No. Spring water; never freezes No ice troubles; well water	No
ne		No	No					.,_	No	No	No
.	None	No	No No					No No	No No	No Never noticed . No ice on standpipe Feb.24.	<i>Nb</i>
			No No	Not perc	Do no:	KNOW		No	No	No	1 16
z/	Riser Encased	No	No No	6"-8"	Never I		much	No No	No No	No No	No No
	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		No No		No .	data 33 Mar. 4	1	No	No No	No No	No No
	None None		No No	3"-12"		35 (1011.4.	1-15"	No No	No	Leaks badly due to poor construction.	146
2,	Riser Encased	1.6	No	Ver	y little	Not me	asured	No	No No	No	No No
ed n		No No	No No	None		12"		No	No	No ice ever forms. 1893 ladder torn off by ice. Not replaced	100
		No	No No	12"-18" Some	l <i>None</i> ice but n	18" of measu	None red	No No	No No	No Some or two small rods attached to force main, broken off by ice.	No No
27		/"	No No		noticed	. , , , , , , , , , , , , , , , , , , ,	Coating	No No	No No	. NO -	No
-	None	1/0	No			Very thin	ļ.,	No	No	No. Water level fluctuates.	N6 No
odi nk or cain	None tai	No Xeeps out a rlow	No No	None 24"-48"	4"-12" N& E Sides	72"	illy none 36"	Rarely 6"-24"	Yes (5,	No. Often cracks like a pistol shot. Has frozen solid on top	No
		Yes Neces	No No	2"		4"		No	No No	No No	No No
cc.	None None	Court diff.	No No		lo trouble	with ice		No No	No No	No. Frequent pumping prevents	No
,	None	No	No	M	one	No	ne	No	No	No	Cant say
æa	None	No Probably	No No		heavy ice fo			№ <i>№</i>	Yes (6) No	No. Probably more ice on N.s-W. sides than on S. Yes. By freezing of seepage to autside wait	No
Tic in	None		No No	None	Very little 1"-4"	None	Very little	No No	No No	Yes. By freezing of seepage to outside wait. No	15. NO NO
	Riser Enc ased None	Α'?	No No	No		measured No	ice	No	No	No No	No Favors nood t
חט	None Riser Encased	Nο	No No	2*	Dont 4"	Кпоw 6"- 8"	10*	No	(7) No	No. Standoune shut off in case of fine	No
	(Supply Pipe Encased	No	No	Very lif	tle ice	3"	A few inches	No	No	No bottom pipe free	160
	None Riser Encased		No No	No re	Dont cords	know 6° i°loating	None	No No	No No	No No	No
CE.	R SUPPLII	ES W	TH I	UNCOV	ERED .	STAND	PIPES				
í	None	λ'ο	No	Λίο	ne			No	No	No. Ice formed only once in 10 years.	Yes, think they should be covered
۱			No No	18" floating		24"		No	No	No	1 1/0
	None		No No			72"	1/2"	Yes 24±	No	In 1894-95 ice 1/2" thick tore out ladder for about 30 ft.	No
			No				<i>36</i> °	No No	No No	1/2	No
-			16				JU .	Λ6	No	No noticeable damage, great strain; believe if should be covered." No	No No
ı			No No		i			No No	No No	No No	No No
	None		No Yes	60°-96″	Unknown	96*-120*		Yes (8)	No	No No	No Yes
			No No		one		one			Never any ice.	No
			No	No	en in center ice for s	everal ye	No rars	24 - 20 yrs. ago 24	No	No. Water kept below 10 ft of top. No ice in recent years. No. In winter do not fill pipe up.	No No
	Vone		No No	6 - 12 No	ice	No	ice	24	No	No. In winter do not fill pipe up. No trouble not in use now	No No
	None None		NO NO	νο	ice	<i>No</i> 1	ice	No	No	No No	No No
	None None		No No			ļ	36 cakes 36	Yes Iz	No No	No No	No
	None		No		Do not	Know	صر	No No	No No		l No Do not know

METCALF & EDDY										la-	
Consulting Engineers					E	XPEF	RIEN	1CES	WIT	TH ICE	11
BOSTON-MASS.		DAT	A OBTAINEL	BY	ME	TCALF & E	DDY.	FEB MAI	R. 1920 FA	ROM AND BY TH	E Cc
						F	ī. ·	T		1	
Place	Authority	Date of Construction	Material of Construction	Diameter - Feet	Height - Feet	On ground or on tower	Height of tower or hill.	Location	Kind of roof	Encasing tower	Encased for Architectural
		8		2	`		Ĭ.				41
					GRO	OUP II A	. <i>S</i>	URFACI	E WATE	R SUPPLIE	ES V
1. B 1/V	G.A.Angierson, Wart Co	n. 1909	Stecl	40	85	Ground	ï	Exposed	Wooden	Brick 12 ft larger than pipe	Yé
I. Buffalo, N.Y. 2. Hamilton, N.Y.	G.L.Waldron, Supt	11. 1303 1. 1895	Steel	37	37.5			Exposed	Concrete	Brick 2ft from shell	Air
· 3. SYRACUSE, N.Y.	Water Dept.	1910	Steel	66	51	Ground		Exposed	Conc.dome	(5)	Ν
4. MILWAUKEE, WIS. MAIN STA.	H.P. Bohman	1872	Wrought Iron	4	125	Ground	İ	Exposed	Tin	Stone tower	169
5. Milwaukee, Wis. Booster Sta 6. Attleboro Mass.		1886	Steel Reinf.Concr.	15 50	173	Ground Ground		Exposed Exposed	Tin GustavinoTile	Brick tower	1
6. ATTLEBORO, MASS. 7. EDMONTON, ALBERTA. (7)	Water Dept. Water Dept.	1906	Steel	24	36	Tower	90 ft.	Exposed	Shingles .	Encased in wood	for pa
8. HUMBOLT, SASK.	C.A.Cutting, Supt.	19/2	Steel	20	80	Cement pier	8 ft. 6 in.	Exposed Bushes EN Exposed #3	Lumber on Care	Encased in wood sing 5 Ply wooden shell	(a)
9. Saskatoon, Sask.	G.D.Archibald, City Eng	1908-10	Stee!	20	80	Conc. found.	5 ft.	In open	ω	Waod'	A2
					<u></u>	77.			- 14/	0	
						OUP II E		URFACE		R SUPPL	<u>IES</u>
i. ALCONAGO, MICH.	Al. El. Lt. 6- W.W.		Cdus/	20	60	Tower	40 ft.		Iron	None	1
2. MENASHA, WIS. 3. PARRY SOUND, ONT.	J. H.Knester, Supt. Geo. Murray, Eng.	1903 1914	Steel Steel	15 36	60 27	Brick toner	60 ft. 50 ft.	Exposed Exposed	Steel Iron	None None	1
4. VICTORIA. B.C.	Water Dept.	1909	Conc. stee! lines			Tower	70 ft.	In open	Concrete	115776	1
5 MANISTIQUE MICH.	H. Erickson, Supt.			18	20	Tower	80 ff.	Exposed	Stee!	Riser encased	45
6. STAMBAUGH, MICH.	Water Dept.	1908	Steel	20	20	Tower	80 ft.	Exposed	Stee!	None	A2
7. WATERLOO, N.Y. 8. FARGO, N.D.	H.S.Kinney, V.P. Water Dept:	1913 1904	Steel Steel	20 20	50 100	Tower Concr. base	100 ft.	Exposed'	Steel Shingle	None	A2 A2
9. PEEKSKILL, N.Y.	1. G. Roake, Supt.	1910	Steel	24	60	Ground	Ì	Exposed	Steel cone	None	\ \hat{\chi}
10. BROCKTON, MASS 3.5.4.	H. Kingman, Supt.	1908	Steel	19	19:8		80ft:4in	Exposed	Wood	1	1
II. BELLEVILLE, ILL.	C.M.Horner	1895	Stee!	23 %	125	Grouna'	ļ	Exposed'	Stee!		1
					GR	OUP II C	- 51	JRFACE	WATE	R SUPPLI	FS
I. ALEXANDRIA BAY, N.Y.	Edutor Cod	1903	Wrought Iron	20	80	Ground	1		None		
1. ALEXANDRIA BAY, N. 1. 2. LYNN, MASS.	Edw. Lee , Supt. R.J. Newsom ,Sup		Steel	50	35	Ground	ļ	in open Exposed	None	None	
3. MASSENA, N.Y.	St. Lawrence W.Co		Steel	20	70	Ground		Exposed	None		l
4. WINTHROP, MASS	L.R.Dunn, Supt.	1910	Steel	40	100	Ground		Exposed	None	None	
5. CANTON, N.Y.	L.R.Smith	1889 1886	Wrought Iron Steel	20 25	70 100	Ground Ground		Exposed	None None	None	
6. ABINGTON & ROCKLAND 7. WATER WORKS, ROCKLAND, N	Water Works, Mass Water Works		Cement	50	100	Ground'		Exposed Exposed	None		į
8. South Pittsburgh, Pa.	E.L.Keane.Mar.W.Q	1. 1905	Steel	25	:50	Ground	i	in Open	None	None	
9. JOPLIN Mo.	A.B.Lynn, Wat. Dept.		Steel	15	85	Ground		in Open	None	None	
10. ONSET, MASS. 11. CHICOPEE, MASS.	E.D. Eldridge, Supt. Water Dept.	1894 1893	Steel	20 55	40 60	Tower Ground	63 ft.	Exposea'	None None	None (8)	
12. LEXINGTON, MASS.	EL.Locke, Supt.	1912	Wrought Iron Concrete	30	105	Ground	ł	Exposed Exposed	None		1
13. SAUGUS, MASS.	A.F. Hart Supt	1913	Steel	45	85	Ground		Exposed	None		1
H. LINDSAY, ONT.	Water Dept.		Wrought Iron	16	110	Stone found.	2 Ft.	Exposed	None	None	No
15. KINGSTON, ONT. 16. St. Joseph, Mich.	C.C.Folger, Mgr. Water Dept.	1890 1892	Steel	40 15	80 100	Stone found	3 ft.	Exposed (3)	None None	None	No
17. QUINCY, MASS.	Water Dept	1892	Wrought Iron	35	60	Ground		Exposed	None None	None	No
18. WEYMOUTH, MASS.	Waner Dept.	1885	Wrought Iron	40	75	Ground		Exposed	None		‴
19. BROCKTON, MASS 1.	H.Kingman, Supt.	1890	Iron	62	59			Exposed	N'one	i	1
20. BROCKTON, MASS. 2. 21. ROCHESTER, N.Y. WACO.	H.Kingman, Supt.	1905 1904	Steel Steel	75 150	35 20	Canada		Exposed	None None	None	1
21. ROCHESTER, N.Y. WACO.	G.H. Bliven, Supt. Water Dept.	1904	Wrought Iron	20	20 90	Concr. found. Ground		(4) Exposed	None None	None	
22. RUTLAND, MASS. 23. EAST ST. LOUIS, ILL	C.M. Horner, Supt.	1896	Stee!	16	100	Ground		Exposed	None		l
ZA EDGEMONT, E. ST. LOUIS, ILL.	C.M. Homer, Supt.	1908	Stee!	66	30	Ground		Exposed	None		1
25. MACLEOD, ALBERTA. 26. GREAT FALLS, MONT.	G.H. Aliham, Supt.	1907	Stee!	22	40 60	Tower	92 ft.	In Open	None	None	1
27. LETHBRIDGE . ALBERTA	M.L. Morris, C.E. H.W.Meech, Com.Pub.W	1907	Steel Steel	30	60 80 75	Ground Ground Conc. Found		Exposed Exposed Exposed	None None None	None None	1
28. BUFFALO, N.Y. I. (WESTERN	(1903	2.20	40	80	. , ,		,			
29. BUFFALO, N.Y. 2. NEW YORK	H.F. Huy, Gen.Mgr.			25	50			· ·			
31. VILLE ST / AUBENT ONT	M. Marcel. Supt.	1911 1905	Stee!	80 22	15 100	Concr. base	9f+	In Open	None	None	
32. PORT ARTHUR, ONT.	L.M.Jones . City Eng.	1905	Steel	25	65	Ground	""	Exposed	None	None None	
33. ANTWERP, N.Y.	C.F.Burtiss , Supt.	1895	Wrought Iron	20	50	Ground		In Open	Nane		No
34. MT. VERNON, N.Y.	H.E. Wolbert, Supt.	1886	Steel	25	125	Ground	Ground level	Exposed	None	None	Ι.
35. MEDICINE HAT, ALBERTA. 36. IRONWOOD, MICH.	R.B.Pyper, City Eng. Water Works	1890	Stoel Wrought Iron	35 30	70 50	Concr. base Ground	level"	Exposed Exposed	None None	None None	No
37. St. Joseph, Mo.	C.H.Taylor, Supt.	1900	Steel	50	<i>55</i>	Ground		Exposed	None	None	1
38 SENECA FALLS, N.Y.	Water Dept.	1900	Steei	30	100	Ground		In Open	None	None	l
39. PEMBROKE, ONT.	J.P. Howe, Town Eng.	1893	Steel	20	60	Ground	}	Exposed	None	Nane	l
40. MARINETTA, WIS.	Water Dept	1912	Sicel	40	20	Ground	<u></u>	Exposed	None	None	l

(I) Wood fastened to stock braces attached to pipe, 2 ft. air space. (2) Foundation top level with the street grade. (3) T (5) Brick tower stone trimmed supports roof. (6) in 1914 6" brick wall 2" air space, paper and asphalt lining, sealed too and (8) Tank unprotected but tower of hard pine entirely encased. (9) Partly but also protection against frost. (b) Partly to prever jacent firehall applied to vertical pipe for frost protection. Now is to Nat. 15. (3) 21% frost platform around scholade of top, of standpipe to break up the ice. (15) Waste water to distribution mains and reful., water fluctuates.

WITH ICE IN STANDPIPES											
20 FF	ROM AND BY TH	E COUR	TES	OF THE	WATER	WORKS	SUPERIN	TENDE	N75.		
d of rf	Encasing tower	Encased for Architectural effect only ?	Is standpipe out of service in winter?	Thickness in ordinar On top of water	of ice by weather On inside of shell		of ice in inary weath On inside of shell	Docs ice project above pipe ?	is artificial heat applied ?	Has pipe suffered injury from ice ?	le additional st of 50% to 18 for protection.
VATER SUPPLIES WITH ENCASED STANDPIPES									€8.5		
den	Brick 12 ft larger than pipe	Yes	No	None	None	None	None	No {	office of	at No.	
rete dome	Brick 2ft from shell (5) Stone tower Brick tower	λο λο {(9)	No No No	None		None 2"-6"		No No No	No No No	No No never more than skim of ice an SNo. When ice freezes solid, salt is used	Yes, would prevent treesing No No
wino Tile gles roof er on cas	(6) Encased in wood ing 5 Ply wooden shell	(10) For protec (11)	No tian No No	9"-10" N	 20e	24 thick:	er found in etandolpe in blocks	No No	No (i2) No	No. Since protection in 1944 No Not during past 2 years	No No No
W	Wood'	70	No	24"	0"12 at to	0	L	160	1/0	No J.	Yes
IATE	R SUPPL	ES W	1TH	Roof	ED ST.	ANDPI	PES				
·/ rete	None None None		√0 √0 √0 √0	None None 24	24" 36" 24" No	None	24°. 42°	No No No	No No No	Yes. Shut off and did not drain. This winter splitniser, will cover and install boiler to keep it open. No. No.	,Vo No No
/	Riser encased None	Λ5 Λο	λ'ο Λο	4"-6"	12"	10"	24'	Sometime No	No No	No. Cut out ice.	№ № №
√	None	No	No	Dont know	1 10"	!	70"	No	No	Yes. In 1917-18 water frese; inject steem	No
gle	None	ΛЭ	No No	None His yea None	1 N. Side	{ 15 ft overtile filled up None	Ï	No No	No No	No	No No
2' 1'			No No	No	 <i>Data</i>	No	Dat a	No No	No No	No No	No Nb
ATE	R SUPPLI	EG 1//	ITU	LINCON	EPED	STAND	PIDEC	L			
A / L	None	3 /1	1/0	10 ft.	3"	JIANU	FIFES	6-8 ft.	No	No. Ice projects sometimes in spring.	No
9			No No	Negligibie	None	About 24	{thin around tedge anily a	110	No No	No No	No
•	None None		No.			18"-24"		Twice 3 A	4/0	No. Paint baidly scraped off 20 ft below top	No No
	TIOTAL		No No		Do not	know	t	Sometim	e No	No '	No
•	None		No	No	ice	So	me ice	Sometim No	No		No lot in this climate
	None None (8)		No No	5"-10"	Do not	Know 18"	15" 5	No Seldom, 3)		No. Water kept fluctuating	No No
•			No No			.	,	No No	No No	No (14) Water level 25 ft. below top, seldom ice	М
:	None	No	No No	24"	8"-11"	About 48	24" or less 48" N. side 12" 15" S. side 24" Near botto 2" 3" on tog	No September	No Se No	No. Water kept high toward spring, fluctua	No rtes No
:	None	No	Νο Νο			İ	24 Near botto 2 3 on top	m Nevel Sceni Sometin	to No	No No	No No
	None	No	No No	6" Floating			"	No		No	No
		-	No No	6 / Journey		6" 6"	1	160	No No	No. May have taken off a little paint.	No No
•	None		No	26"	15" 18"	36"	24*	No No	No No	No. Máy have taken off a little paint. No	No No
			No No	No		16	Dartar	{ rezent No	NO NO	No No	No No
,	Nane	50	No metim	es 12	Data - 15	24	Data -30	No 2 ft.	No No	No No	Λο Λο
	None None		\% 1%	(Thin	1522	Thin	48. 36.	№ 18 -36 18 -36	No No	No. Overflow pipe has been blocked	No No
					7	Some ice Broken ice	12"-24"	Sometim No		No No	No No
,	None				12"	72"-96"	24"	No	No	No	No No
	Nane	No Or	e Wim		43" 24"	<i>®</i> *	48° 36'-48'	10-15 ft 2-3 ft	No	No Yes. Leaks at rivets.	Yes
;	None		Λο Λο	Тор оре п 12"	None	Ореп 36	None	10-15 ft. Once 2 ft.		No loe ripped off inside angle iron at top.	No No
;	None None	No	No No	12" Don. 12"	8-12"	None 16-18	About 18	No 6-12"	No No	No No	No No
;	None None		No No	6"8"	Dont know	24"	Dont know	No No	No No	No (15) Don't think so	es but Co yould not do it
,	None None		No No	6"8"	None	18"	24° N.W. side None	No No	No No	No No	No.
		L		<u> </u>	L	L	L	لــــــــــــــــــــــــــــــــــــــ		<u> </u>	

the street grade. (3) Three sides exposed, North protected by buildings. (4) Exposed, sheltered some by trees. half lining, sealed too and viero holes. (7) Recently sold to Alberta government, now excited and inuse at Red Deer, Alberta, rost. (8) Partly to prevent spalling of concrete. (1) Architectural effect combined with service. (12) Steam line from deform around outside of top, overflow freezes to this, have seen ice 18' thick in pipe. (14) Row of spikes 6ft from top of inside tustes.

and more or less all around. The top ice is moving either up or down all the time and breaks into cakes, and rolling around they grow bigger, some 3 feet, some smaller.

St. Joseph Water Company, Missouri; C. H. Taylor, Superintendent. The standpipe at the reservoir is used very seldom and only in case of fire. When the weather becomes cold enough to form ice on the standpipe, we at once open the by-pass around the check valve and permit the water in the standpipe to waste into our distribution mains, the rate of flow of the water through this by-pass depending on the temperature.

The lowering of the water in the standpipe keeps the ice cake on top of the water constantly broken up into small cakes and slush ice, this being a 50-foot diameter by 55-foot high standpipe. In extreme weather we permit the water to waste out of the standpipe until perhaps we have lowered the head from 10 feet to 15 feet from the point where we started. We then pump water into the standpipe, bringing it again up to the top of same or to the overflow and usually during extreme weather we are obliged to refill the standpipes weekly. The only precaution necessary to protect the standpipe from damage during cold weather is to keep lowering the water in same sufficiently rapidly to prevent the surface freezing solid enough that the surface cake will break when the water level is lowered underneath same. It is also very essential when the standpipe is ringed with heavy ice not to permit the water to lower too far at a time when the temperature is rising for fear that this inside lining of ice when very heavy will fall, in so doing, cause undue strain on the structure of the standpipe.

St. Joseph Water Works, Michigan; F. A. Bunks, Superintendent. We have had the ice shoot up over the top of the pipe in the spring time, due to the station allowing the water in the pipe to rise above the danger point.

We have had trouble with the ice when we try the policy of pumping the standpipe full of water and then shutting down the pumps until the pressure dropped sufficiently. We have for the last 5 years maintained an even water level in the pipe during the winter (or as nearly level as possible) with the result of no trouble with the ice. Domestic pressure is 40 pounds per square inch. For fire we cut out the standpipe and pump direct, with a fire pressure of 80 pounds.

Menasha Water Works, Wisconsin; John H. Knester, Superintendent. We installed an 1800 gallons per minute centrifugal (pump) this winter that held the head too steady and ice formed on top of water; also our riser pipe froze solid and split four lengths, 48 feet, which we have just renewed at a cost of over \$500. I believe in our case that we will cover riser pipe with felt frost covering and I think we ought to put in a hot water boiler of about 500 feet radiation capacity in which to burn hard coal, this to keep riser pipe open and to keep ice from forming on top of water and keep ice from getting too thick around shell; this heater to be connected to a tap at lowest point of riser pipe and also just above boiler. This will give circulation down to below frost level. This arrangement will cost less in operation and maintenance than going to extremes in cost for frost coverings and housing. . . . If we don't put in some sort of heating we will have to drain tank and piping and lose the advantage of storage for emergency.

Manistique Water Works, Michigan; H. Eriksen. During the winter months, about once a week we cut out the ice formed in standpipe (which formation begins at the inlet to the tank) in the following manner:

We close the valve at one side of the tank and open the valve opposite it, which permits the water in the riser and standpipe to empty into a sewer. The force of the moving water very effectually clears out any and all ice that may have formed, either in the standpipe or riser. This operation takes about 25 minutes.

Milwaukee Water Works, Wisconsin; H. P. Bohmann, Superintendent. At the North Point Pumping Station standpipe, we have no ice trouble in moderate winter weather, as the fluctuation of the water in the standpipe keeps the ice broken. When the temperature is at zero or below, ice at times becomes solid and just as soon as it begins to get solid, a pail of salt is dumped on the ice which eats through the ice in a very short time. The formation does not give us trouble, as it gradually melts in early spring.

At the High Service Pumping Station, the greater fluctuation of water keeps it open most of the time, otherwise salt is introduced in the same manner as at the North Point Pumping Station. Where the salt eats through the ice I should judge it is anywhere from 2 inches to 6 inches in thickness, tapering down to nothing. The distance from the top of the ice to where it tapers away is anywhere from 10 to 15 feet.

By keeping an opening with salt, we have avoided ice troubles at all times.

With respect to additional cost of from 50 to 100 per cent for encasing or covering a standpipe he says:

It would be justified in this city as bare standpipes are not ornamental and our standpipes are located in a fine residential district.

Port Arthur, Ontario; L. M. Jones, City Engineer. We have a standpipe here and have also encountered some ice troubles.

Our standpipe is 25 feet in diameter by 65 feet high and holds approximately 200,000 imperial gallons. It is built of steel and was constructed in 1904. It is situated on the highest ground in the city and rests on a concrete foundation supported by solid rock. The top is 278 feet above the supply level. When it was built, the base was at a considerably higher elevation than any other building, but since then the residential portion of the city has grown considerably in the direction of the hill top, so that there are now a large number of houses on the same level as the base of the standpipe. One large house and a school have the plumbing fixtures located at an elevation about 30 feet above the standpipe base.

When the standpipe was first built the population was small and the system of piping new. The pumps were operated through the day and after midnight were closed down, the consumers being supplied from the standpipe. In this way the water was changed daily at least. As the population and number of consumers grew and the system increased, the pumps were kept in service longer during the day, but they struggled to keep water on the hill top, the consequence being that the water level in the standpipe kept fluctuating to such an extent that the water was continually changing.

During these periods we had no trouble with ice. The writer remembers seeing the ice 2 or 3 feet above the top of the standpipe, floating in the water, but this was in the spring after it had loosened from the sides.

Later on, the city grew in all directions and the standpipe had to be kept full nearly all the time to ensure a supply at reasonable pressure to the consumers in its immediate vicinity. Also a power sub-station was located quite near it and this had to be protected from overflowing. In the old days when there were no houses near, it did not matter if it did overflow. But subsequent development would not permit this.

New pumps were installed at the main pumping station and a booster pump was set in the system half way up the hill to help out for fire fighting. This booster was automatically controlled. A Golden-Anderson altitude valve was placed on the inlet to the standpipe. When the water dropped in the standpipe to a level 12 feet from the top, the pump cut in and filled the standpipe, or the valve can be closed at any water level. Our new pumps at the main station were of greater capacity than actually required at present and the standpipe was therefore kept full nearly all the time. In short, there was very little changing of the water, with the result that the standpipe froze over solid and the sides were lined with ice about 4 feet in thickness. We first noticed trouble when the water receded from the ice and gave us trouble with the controlling mechanism of the booster pump, probably due to vacuum conditions set up between the water level and the ice level. At any rate when we cut a hole in the ice the trouble disappeared. I may say that there was quite a rush of air when the hole was cut. For the balance of the winter (1914 and 1915) we kept the ice clear of the top of the standpipe.

The following winter we cut the standpipe off the system entirely but experienced considerable trouble, as it proved to be quite a balancing feature on the system.

We have since that time kept it on the system but have not allowed it to freeze over solid, but keep a hole about 12 feet in diameter at the center of the ice covering. This requires attention about twice a week, but we get no other trouble.

My opinion is that to get the best service, the standpipe should be completely housed in and some degree of heat be introduced to keep the water from freezing. A standpipe is constructed of a capacity sufficient to perform a certain duty. It is questionable if the reduced storage capacity (in our case it is reduced 50 per cent or more) due to ice formation is ever considered. In our country the ice condition prevails at least five months in each year or nearly 50 per cent of the time. In order to get the maximum benefit of the expenditure, the cost should be increased to secure a proper covering and thus receive 100 per cent return for the investment. Aside from this there is always the serious danger due to the expansive effect of ice on a structure of this kind.

Humbolt Water Works, Saskatchewan; C. A. Cutting, Superintendent. Contemplate drawing about 50 gallons per minute from condenser basin and pumping into tower, the more gradual the better, to minimize contraction and expansion of joints in pipe.

. . . Allow the level to remain at 60 feet, then increase to 70 feet, which melts ice which is under water. If tower is kept full all the time no op-

portunity is afforded for temperature in newly pumped water to act on ridge of ice.

Also divide pumping up, say, over 4-hour periods.

Saskatoon Water Works, Saskatchewan; C. A. Cutting, Chief Engineer (formerly). A 250-horsepower boiler was fired and a 2-inch steam pipe let loose at about 100 pounds pressure without avail. Previous to this, city water was pumped through a small condenser of 400 feet surface.

North Battleford Water Works, Saskatchewan; M. D. Cadwell, Superintendent. The writer has had twenty years experience in the West with water systems and is fully convinced that any tower unhoused is entirely unsuitable for a climate such as prevails in Western Canada during the winter months.

No trouble due to fact that tower is completely housed and further to the fact that our water system is supplied with warm water, the initial temperature of which is approximately from 60° to 70°, usually from the last day of February to the end of March or later, as the conditions may require.

Prior to the commencement of the warm water supply, which is taken from the cooling basin at the power plant, we always found a quantity of ice floating on the water in the standpipe. To the best of the writer's knowledge, the same has never adhered either to the wall surface in any quantity nor has it become lodged at the top of the tower, but has always floated on the surface of the water.

The writer understands that a number of towers have been wrecked due to the fact that the ice adhered to the walls or the top of the tower and fell, due to increased temperatures, when the water was at a low elevation in the tower.

CONCLUSIONS BASED UPON RECORDS SUBMITTED

- 1. Open standpipes have been operated successfully in the northern United States by water works having surface, as well as by those having ground-water supplies, in spite of some trouble due to the formation in them of ice during the cold winter months.
- 2. This statement is true also of some water works in Canada, though its climate makes the covering of standpipes more generally necessary than in the northern United States.
- 3. Past failures of standpipes have been frequent and serious enough, however, to make careful consideration or analysis of conditions of location, exposure, method of operation, circulation and variation in rate of water demand, desirable, with a view to determining whether the financial condition of the works will justify the encasing or roofing of the standpipe, make necessary the assumption of the hazard of difficulties or injury to be anticipated from ice formation, or compel the abandonment of the idea of the use of a standpipe.

- 4. Structures within the standpipe, such as ladders and overflow pipes, are to be avoided, as they are likely to be torn down by the floating ice sheet.
- 5. Heavy variation in demand inducing good circulation within the standpipe generally minimizes the formation of ice. The maintenance of a water surface substantially below the top of the standpipe seems to tend in the same direction. But when a heavy ice sheet has formed on top, practical experience or perhaps fear of trouble has led superintendents to try to maintain the water level as nearly constant as possible, particularly when the melting of the ice sheet is expected, in order to prevent the fall of a heavy mass of ice into the water below it, with piston-like shock and imminent danger of collapse of the entire structure.
- 6. With increase in diameter over 30 to 40 feet, troubles from ice appear to decrease. Often they do with standpipes of smaller diameter, though probably for different reasons.
- 7. In extreme cases salt has sometimes, though rarely, been used on the surface of the ice sheet, to keep it open; holes have also been chopped in it to prevent suction from being developed between the ice sheet and the dropping water column, which would tend to cause the fall of the ice. In Canada the expedient of pumping some condenser water into the standpipe, to raise the temperature of the supply, has also been used successfully.
- 8. Usually the warmer incoming water at the bottom of the standpipe tends to prevent the formation of ice at this point, or even in the lower part of the structure.
- 9. In extreme cold, ice often forms in a cylinder around the inside of the standpipe, as well as in a sheet covering the water surface in the standpipe.
- 10. There is substantial danger from the partial melting of the ice cylinder on the southerly side of the standpipe, under the warmth of the rays of the sun and from the refreezing of the water thus melted, held between the steel shell of the standpipe and the vertical annular ice cylinder within it, with undesirable if not dangerous expansive force.
- 11. Ice is reported to have projected above standpipes from 10 to 20 feet in extreme cases. These amounts seem almost incredible, but at least one photograph is available showing the projecting column of ice to have been nearly equivalent to two rows of plates, or 10 feet in height, above the top of the structure. This case

developed on the south shore of Lake Michigan in a standpipe 16 feet in diameter and 100 feet high. How far down it extended under those conditions, is unknown. The danger to the structure inherent in the fall of such a slug of ice is obvious.

- 12. A heavy ring of ice near the top of the standpipe, with solid sheet of ice covering it, is common even when the vertical cylinder of ice next the wall of the structure tapers rapidly toward the bottom.
- 13. The roofing of the standpipe (without encasement of its walls) seems to have been generally effective in preventing the formation of a heavy ice cylinder or floating ice sheet within the standpipe, particularly where ground water supplies are used. The fact that a greater percentage of standpipes supplied with ground rather than with surface water have been roofed may be due to the greater need of excluding sunlight from ground water, to prevent the growth of algae.
- 14. The complete covering of the structure, leaving a space of 30 inches or more between the standpipe shell and the encasing material, for painting, is the most effective and desirable protection against trouble with ice in exposed northern sites, particularly where the water is cold, the circulation slight and the financial considerations involved are not prohibitive. The application of heat is sometimes resorted to in the coldest weather, to prevent freezing of the riser pipe, where the standpipe is elevated.
- 15. With reference to the age of these standpipes the following notes may be of interest. Of the 118 tanks the ages of which are known, 64 per cent are of steel, 20 per cent wrought iron, 12 per cent reinforced concrete, 4 per cent of wood. The ages of the steel tanks range from 4 years to 30 years, the average age being 17 years. The ages of the wrought iron tanks range from 17 years to 48 years, the average age being 31 years. The age of the reinforced concrete tanks is from 6 years to 20 years, the average being 11 years. The age of the wooden tanks is from 7 years to 30 years, the average being 23 years. In interpreting these results it is to be borne in mind that the wrought iron is the oldest material used; that steel came into general use at a slightly later date, and that the use of reinforced concrete for standpipes is of comparatively recent origin. The data concerning the wooden tanks are not sufficiently complete to be of significance.

ADDENDUM

Since compiling the tabulation upon "Experiences with Ice in Standpipes" the following interesting information has been received from Mr. S. E. Killam, Superintendent of Pipe Lines and Reservoirs, Water Division of the Massachusetts Metropolitan District Commission, relative to three of its standpipes, all of which receive their water from surface supplies.

	"ARLINGTON" AT ARLINGTON HEIGHTS	"BOSTON" AT BELLEVUE HEIGHTS	"QUINCY" ON FORBES HILL
Date of construction (approxi-	1894	1914	1900
mate)	1		1
Material	Wrought iron	Steel	Steel
Diameter (feet)	60	100	30
Height (feet)	40	44	64
Foundation	Masonry	Masonry	Masonry
	base	base	base
Position	Exposed	Exposed	Exposed
Kind of roof	Conical, rest-		bservation roof
	ing on	of tower	
	standpipe		
Method of encasement	None	Masonry	Masonry
		tower with	tower with
		4 ft. space;	3.25 ft.
		wall 3 ft.	space; wall
		thick at	4.75 ft.
		base	thick at
			base and 2
			ft. at top
			below cor-
			nice
Was encasement designed for			
architectural effect only?.,		No	No
Is standpipe cut out of service			
in winter?	No	No	No
In ordinary weather how thick			
does ice form on top of water			
in standpipe?	6 to 8 in.	2 to 4 in.	2 to 4 in.
On inside of shell?	None	None	None
In extreme weather how thick			
does ice form on top of water			
in standpipe?	8 to 12 in.	6 in.	6 in.
On inside of shell?	None	None	None

	"ARLINGTON" AT ARLINGTON HEIGHTS	"BOSTON" AT BELLEVUE HEIGHTS	"QUINCY" ON FORBES HILL
Has ice frequently projected above standpipe?	No	No	No
Is artificial heat ever applied?	No	No	No
Has standpipe ever suffered serious injury from ice? Do you think under conditions of your works an additional cost for encasing of from 50 to 100 per cent of cost of stand-	No*	No*	No*
pipe itself, is justified?	Yes	Yes	Yes

^{*}Although interior coating has been injured by movement of ice.